
Failure of left main gear, Boeing 757-223, August 24, 2003

Micro-summary: Failure of the left main gear bogie on this Boeing 757-223 taxi-out.


Event Date: 2003-08-24 at 1110 EDT

Investigative Body: National Transportation Safety Board (NTSB), USA

Investigative Body's Web Site: <http://www.nts.gov/>

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		NTSB ID: MIA03IA168		Aircraft Registration Number: N609AA	
		Occurrence Date: 08/24/2003		Most Critical Injury: None	
		Occurrence Type: Incident		Investigated By: NTSB	
Location/Time					
Nearest City/Place Miami		State FL	Zip Code 33132	Local Time 1110	Time Zone EDT
Airport Proximity: On Airport		Distance From Landing Facility:		Direction From Airport:	
Aircraft Information Summary					
Aircraft Manufacturer Boeing		Model/Series 757-223		Type of Aircraft Airplane	
Sightseeing Flight: No			Air Medical Transport Flight: No		
Narrative					
<p>Brief narrative statement of facts, conditions and circumstances pertinent to the accident/incident:</p> <p>On August 24, 2003, about 1110 eastern daylight time, a Boeing 757-223, N609AA, operated by American Airlines Inc. as flight 1163, a Title 14 CFR Part 121 scheduled domestic passenger flight, had a failure of the left main landing gear truck beam, while taxiing for takeoff at Miami International Airport, Miami, Florida. Visual meteorological conditions prevailed. An instrument flight rules flight plan was filed. The airplane received minor damage. The two airline transport-rated pilots, four flight attendants, and 163 passengers reported no injuries. The flight was originating at the time, and was en route to Chicago, Illinois.</p> <p>The first officer stated that during preflight examination of the airplane he didn't see anything wrong with the aircraft and it was deemed suitable for flight. They closed the doors and blocked out at 1055. After receiving the taxi clearance, they proceeded on "Mike" taxiway to runway 9L. During taxi, the aircraft suddenly dipped left and skidded to a stop. They assessed a possible tire blowout and after contacting ground control the aircraft behind them confirmed it was the left outboard main tire and it was smoking. They immediately called for fire equipment, which responded to the aircraft. They shut down the aircraft and called ramp control, maintenance, and flight dispatch to coordinate. After the fire crews visually inspected the aircraft they reported the left main landing gear had failed and there was no fire or smoke to be seen. Maintenance confirmed that the bogie on the left main gear had failed. There was no threat to safety and they deplaned all of the passengers and crew uneventfully and were bussed to the terminal.</p> <p>The failed landing gear components were initially examined by NTSB on the taxiway on the day of the incident and at the American Airlines maintenance facility at Miami International Airport on August 25, 2003. The left main landing gear truck beam had fractured in two pieces between the aft axle and the truck pivot pin. The fracture occurred about 14 inches forward of the aft axle centerline. The truck beam is P/N 161N1611-6 and S/N 16PE2 according to the aircraft records. According to American Airlines the landing gear was delivered new with the aircraft on July 29, 1996, and had accumulated 7,517 cycles since new. There was no truck beam shield present with the wreckage although the attach straps were present. The brake rods were recovered with the beam and show abrasion damage on the lower portion of the lug where they attach to the clevis of the inner cylinder.</p> <p>The aft section of truck beam had shear lips and river patterns present on the fracture face from about the 7 o'clock position around to the 5 o'clock position. The inner diameter had cosmoline covering about 15 percent of the surface and grease covering about 25 percent of the surface area. A big ball of detached cosmoline was present at the lower end of the beam plugging up the drain hole. There was an apparent impact mark at the 6 o'clock position on the outer surface of the beam. There was no apparent degradation of the primer on the interior surface. On the forward section of the truck beam the fracture was located about 10.5 inches aft of the pivot centerline. There was some cosmoline evident on the inner surface but a majority of the surface was covered by grease. The lower third of the beam was filled with grease. There was no apparent internal primer</p>					
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degradation. Again at about the 6 o'clock position on the outer surface there was an apparent impact mark. The fracture surface matched that for the aft section.

Metallurgical examination of the failed left main landing gear truck beam was performed at the NTSB Materials Laboratory, Washington, D.C. The truck beam assembly was transported to the NTSB Materials Laboratory and initially examined on September 5 and 6, 2003, with representatives from the FAA and American Airlines present. Initial inspections found the truck beam circumferentially fractured between the aft axle and the central pivot point. The mating forward and aft portions of the beam were received along with the installed forward and aft axles and five attachment straps. The following markings were found stamped into the exterior of the forward section of the beam; 161N1611-7 ASSY, 161N1611-6, 16PE2 and 17576. The Illustrated Parts Catalog (IPC) indicated that one strap was intended to hold electrical wiring and the other four to attach a truck beam shield, p/n 161N1710-1 to the underside of the truck beam. The truck beam shield was not received in the laboratory and was reportedly not found on Miami International Airport. The interior surfaces of the beam were entirely covered by an intact layer of primer paint. Further, a corrosion preventative compound on top of the primer covered an estimated 15 percent of the interior surface and a grease like substance on top of the corrosion preventative compound covered between 25 percent and 35 percent of the interior surface. During initial on-scene examinations a large ball of corrosion preventative compound was reportedly found covering and blocking the beam drain hole at the aft bottom of the beam.

The majority of the circumferential fracture was located at approximately 14 inches forward of the aft axle centerline and about 10.5 inches aft of the central pivot centerline. Examinations found that the fractures on the forward and aft piece matched and that no pieces of the beam were missing from the fracture area. Optical examinations of the fracture surfaces, after light cleaning, uncovered shear lips and river patterns indicating that the fracture initiated at the bottom of the beam between the 5 and 7 o'clock positions. Close examinations found features consistent with overstress fractures stemming from both sides of a 2.6 inch-long (circumferential) granular area at the bottom of the beam. From the granular area, the overstress portions of the fracture propagated circumferentially around the sides of the beam and forward near the top, meeting at the top of the beam just aft of the center pivot boss. The overall geometry of the fracture was consistent with beam bending loads producing tension stress on the bottom. The lower surface of the truck beam had several areas of disturbed paint and damaged finishes (top coat paint, primer and plating) due to apparent contact with other objects.

The granular portion of the fracture was located within the largest disturbed area measuring about 3 inches circumferentially and 4 inches longitudinally. The disturbed area was mostly on the forward piece of the beam but also extended onto the aft piece. At different points within this area, the paint, primer and cadmium plating were variously missing. Bare base metal was exposed adjacent to and forward of the fracture but no significant base metal appeared to have been removed. Most of the damage to the finishes was in the longitudinal direction on both sides of the fracture. Scratches, scuff marks and other signatures on the aft side clearly indicated a rearward displacement of the coating materials. Heavy randomly oriented scratches and gouges on the forward side of the fracture overlaid and obscured the longitudinal marks. In addition to the surface damage at the fracture, a portion of the edge of the forward fracture face was dented and deformed upward with the mating area on the aft fracture not damaged. A longitudinal crack was also visible in the damage area on the forward side of the fracture. This crack will be described in more detail later.

In a second area of finish damage the paint was missing and the underlying plating was damaged and displaced at several circumferentially elongated spots in a band between about 4 and 6 inches aft of the central pivot. The damaged spots were generally less than 0.3 inch wide but the largest area measured 1.2 inches long by 0.3 inch wide. Close examinations found the paint missing and the plating displaced mostly in the circumferential directions with flaking paint noted around the edges of the damage areas. A third area of finish damage was noted on the bottom of the beam just

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forward of the jacking knob (approximately 5 inches forward of the aft axle centerline). In this area the coatings were damaged/missing over a large area with indicated movement of the contacting object in the forward direction. To allow more in-depth examinations, sections were saw cut from both pieces of the beam. The sections included the forward and aft granular fracture areas, and the surrounding disturbed finish areas. The removed sections were cleaned of grease and corrosion preventative compound, inspected optically with a stereo microscope, and electronically with a scanning electron microscope (SEM).

Backscattered electron imaging of the outer surface of the beam adjacent to the granular fracture location on the forward side of the fracture uncovered a mottled surface with distinct elemental regions. Elemental maps acquired by energy dispersive x-ray spectroscopy (EDS) established the regions to be predominately cadmium, iron or aluminum. The aluminum regions were found either on top of iron or cadmium. Neither the beam material (AISI 4340M) nor the finishes contained significant amounts of aluminum. However, the base plate of the truck beam shield normally mounted under the truck beam was specified as an aluminum alloy (AA 2024).

Visual examinations of the damaged area adjacent to the fracture also uncovered a "y" shaped longitudinal crack in the bare metal area forward of the fracture. The crack was about 0.7 inches long and both arms of the "y" intersected the fracture near the center of the granular area. The granular area extended completely through the wall thickness of the beam and did not exhibit shear lips at either the inner or outer diameter surfaces. The granular area was made up of fracture regions on two offset planes connected in part by a shear ridge. The outboard region of the granular area was longer and 0.3 to 0.4 inch forward of the smaller inboard region. Micro fracture features within each portion of the granular region indicated crack initiation at heavily oxidized zones adjacent to the outer diameter surface of the beam. Closer inspections established that the oxidized zones were extensions of the arms of the "y" crack. Laboratory bending opened the majority of the "y" crack for examination. Visually, the opened crack surfaces were heavily corroded. Features indicated that the crack initiated at the outer surface of the beam and propagated directly inward. Most of the crack extended about 0.12 inches into the beam wall but a few areas penetrated as much as 0.2 inches. The beam wall thickness at this location was about 0.32 inch. The outboard arm of the "y" crack was not opened but intersected the opened portion at about 90 degrees. SEM viewing of the opened crack surfaces found a heavy covering of corrosion products obscuring some of the fracture details. Corrosion-damaged intergranular fracture facets consistent with stress corrosion cracking (SCC) were found throughout the crack. The laboratory-fractured area adjacent to the crack exhibited a ductile dimple fracture topography. SEM viewing of the granular areas of the circumferential fracture also revealed intergranular facets consistent with SCC. Beyond the granular regions, the fracture surface was composed of ductile dimples. A transverse metallographic section was cut through the forward end of the longitudinal "y" crack after it was opened. Initial viewing in the unetched state revealed cadmium plating on both the interior and exterior surfaces. The plating was discontinuous on both surfaces. Plating thickness averaged about 0.0006 to 0.0008 inch. EDS spectra of the plating established that it was mostly cadmium with a significant amount of titanium consistent with the specified cadmium titanium plating (Boeing finish detail F-15.01), 0.0005 inch minimum thickness. The primer on the beam interior was continuous and measured between 0.0014 and 0.0016 inch thick. Etching the specimen with 4 percent Nitall reagent reveal a fine tempered martensite microstructure throughout the specimen consistent with quench and tempered heat treatment. No evidence of decarburization was noted at either surface. However, small areas of distorted microstructure were uncovered within 0.0006 inch of the beam exterior surface. Energy dispersive x-ray spectra of the beam base metal showed mostly iron with small amounts of chromium, manganese, nickel and molybdenum consistent with a 4300 series alloy steel. Hardness measurements made on the interior surface of the beam ranged from 49 to 52 HRC and indicated a tensile strength slightly less than the specified 275-300 ksi ultimate tensile strength.

As received, five attachment straps were present with the truck beam. Two straps were found around the forward section of the beam, one strap was around the aft section, one strap was loose in the container with the aft section of beam and the fifth was attached to electrical wires. Installation

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drawings show that the truck beam shield is attached to the beam with four straps, two forward and two aft of the truck beam pivot. Each strap contained two clips and bolts to connect to the guard. Chaffing protection tape was applied to the beam at the location of each strap. observations of each strap are presented below. An intact clip is also displayed along with a typical damaged clip and strap. The most forward strap was found about 8 inches behind the forward axle centerline with the T bolt installed on the inboard side with the nut on the upper side. The protective tape was found aft of the strap. The inboard clip was bent aft about 15 and the adjacent area of the strap was deformed rearward. The aft leg in the outboard clip was fractured and the adjacent strap was also bent aft. The second strap from the front was found at 15.5 inches from the forward axle centerline. Witness marks indicated that the strap had moved aft about 0.5 inch along with the protective tape. The bolt attachment legs of both of the clips showed wide separations and rearward deformation in the adjacent part of the strap. The strap was installed with the T bolt on the inboard side with the nut end up. The third strap attached to the beam was located about 4 inches forward of the aft axle centerline. It appeared to be in its installed location with the tape intact and the T bolt on the top of the beam with the nut end facing outboard. The bolt attachment legs of both clips exhibited wide separations of the legs. The strap displayed slight rearward deformation at the inboard clip and significant aft deformation at the outboard clip. The fourth strap was loose and appeared to have been mechanically separated at the T bolt with the nut removed. One clip showed about inch separation of the legs and slight deformation of the adjacent strap. The other clip had a slight separation of the legs with visible twisting. The adjacent strap was slightly deformed. The fifth strap was loose from the beam but attached to the assembly by wires for the wheel transducer. No deformation was apparent on the clips and strap. Shadow lines were apparent in the paint indicating that straps had been installed on either side of the fracture. One was located 10 inches forward of the aft axle and the other was 7 inches aft of the pivot centerline. Remnants of protective tape were found at both locations.

The Boeing model 757 configuration deviation list (CDL), which was current at the time of the incident, lists items that can be missing for flight. The main landing gear truck beam shields may be missing for flight. There was no requirement to inspect the landing gear for damage prior to dispatch with a truck beam shield missing. American Airlines maintenance personnel had not identified the missing truck beam shield on the left main landing gear of N609AA and the item was not on the current list of items missing from the airplane under the CDL.

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Landing Facility/Approach Information						
Airport Name		Airport ID:	Airport Elevation	Runway Used	Runway Length	Runway Width
Miami International		MIA	8 Ft. MSL	NA		
Runway Surface Type: Unknown						
Runway Surface Condition: Unknown						
Type Instrument Approach: Unknown						
VFR Approach/Landing: Unknown						
Aircraft Information						
Aircraft Manufacturer		Model/Series		Serial Number		
Boeing		757-223		27447		
Airworthiness Certificate(s): Transport						
Landing Gear Type: Retractable - Tricycle						
Homebuilt Aircraft? No		Number of Seats: 187	Certified Max Gross Wt. 251000 LBS		Number of Engines: 2	
Engine Type:		Engine Manufacturer:		Model/Series:	Rated Power:	
Turbo Fan		Rolls-Royce		RB211-535-E4B	40100 LBS	
- Aircraft Inspection Information						
Type of Last Inspection		Date of Last Inspection	Time Since Last Inspection		Airframe Total Time	
Continuous Airworthiness		08/2003	1 Hours		25608 Hours	
- Emergency Locator Transmitter (ELT) Information						
ELT Installed? No		ELT Operated? No		ELT Aided in Locating Accident Site? No		
Owner/Operator Information						
Registered Aircraft Owner		Street Address				
		PO Box 619616 MD 5662				
AMERICAN AIRLINES INC		City		State	Zip Code	
		DFW Airport		TX	75261	
Operator of Aircraft		Street Address				
		Same as Reg'd Aircraft Owner				
Same as Reg'd Aircraft Owner		City		State	Zip Code	
Operator Does Business As:				Operator Designator Code: AALA		
- Type of U.S. Certificate(s) Held:						
Air Carrier Operating Certificate(s): Flag Carrier/Domestic						
Operating Certificate:			Operator Certificate:			
Regulation Flight Conducted Under: Part 121: Air Carrier						
Type of Flight Operation Conducted: Scheduled; Domestic; Passenger Only						
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First Pilot Information

Name On File	City On File	State On File	Date of Birth On File	Age 55
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Sex: M	Seat Occupied: Left	Principal Profession: Civilian Pilot	Certificate Number: On File
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Certificate(s): Airline Transport; Flight Instructor

Airplane Rating(s): Multi-engine Land; Single-engine Land

Rotorcraft/Glider/LTA: None

Instrument Rating(s): Airplane

Instructor Rating(s): Airplane Multi-engine; Airplane Single-engine

Type Rating/Endorsement for Accident/Incident Aircraft? Yes	Current Biennial Flight Review? 02/2003
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Medical Cert.: Class 1	Medical Cert. Status: Valid Medical--w/ waivers/lim.	Date of Last Medical Exam: 03/2003
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- Flight Time Matrix	All A/C	This Make and Model	Airplane Single Engine	Airplane Multi-Engine	Night	Instrument		Rotorcraft	Glider	Lighter Than Air
						Actual	Simulated			
Total Time	19378	1924	125	19245	4350	2200				
Pilot In Command(PIC)	15500	1924	95	15408						
Instructor	3200		30	3170						
Last 90 Days	213	213		213						
Last 30 Days	66	66		66						
Last 24 Hours	4	4		4						

Seatbelt Used? Yes	Shoulder Harness Used? Yes	Toxicology Performed? No	Second Pilot? Yes
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Flight Plan/Itinerary

Type of Flight Plan Filed: IFR

Departure Point Same as Accident/Incident Location	State	Airport Identifier MIA	Departure Time 1110	Time Zone EDT
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Destination CHICAGO	State IL	Airport Identifier ORD	
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Type of Clearance: IFR

Type of Airspace: Class D

Weather Information

Source of Briefing: Company

Method of Briefing: In Person

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Weather Information					
WOF ID	Observation Time	Time Zone	WOF Elevation	WOF Distance From Accident Site	Direction From Accident Site
KMIA	1153	EST	8 Ft. MSL	1 NM	270 Deg. Mag.
Sky/Lowest Cloud Condition: Scattered			2500 Ft. AGL	Condition of Light: Day	
Lowest Ceiling: None		Ft. AGL		Visibility: 10 SM	Altimeter: 30.04 "Hg
Temperature: 32 °C	Dew Point: 22 °C	Wind Direction:		Density Altitude: 1200 Ft.	
Wind Speed:	Gusts:	Weather Conditions at Accident Site: Visual Conditions			
Visibility (RVR): Ft.	Visibility (RVV) SM	Intensity of Precipitation:			
Restrictions to Visibility: None					
Type of Precipitation: None					

Accident Information		
Aircraft Damage: Minor	Aircraft Fire: None	Aircraft Explosion: None

Classification: U.S. Registered/U.S. Soil					
- Injury Summary Matrix	Fatal	Serious	Minor	None	TOTAL
First Pilot				1	1
Second Pilot				1	1
Student Pilot					
Flight Instructor					
Check Pilot					
Flight Engineer					
Cabin Attendants				4	4
Other Crew					
Passengers				163	163
- TOTAL ABOARD -				169	169
Other Ground					
- GRAND TOTAL -				169	169

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Administrative Information

Investigator-In-Charge (IIC)

Jeffrey L. Kennedy

Additional Persons Participating in This Accident/Incident Investigation:

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